

Video Article

Fabrication of Silica Ultra High Quality Factor Microresonators

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Abstract

Whispering gallery resonant cavities confine light in circular orbits at their periphery.¹⁻² The photon storage lifetime in the cavity, quantified by the quality factor (Q) of the cavity, can be in excess of 500ns for cavities with Q factors above 100 million. As a result of their low material losses, silica microcavities have demonstrated some of the longest photon lifetimes to date.¹⁻² Since a portion of the circulating light extends outside the resonator, these devices can also be used to probe the surroundings. This interaction has enabled numerous experiments in biology, such as single molecule biodetection and antibody-antigen kinetics, as well as discoveries in other fields, such as development of ultra-low-threshold microlasers, characterization of thin films, and cavity quantum electrodynamics studies.³⁻⁷

The two primary silica resonant cavity geometries are the microsphere and the microtoroid. Both devices rely on a carbon dioxide laser reflow step to achieve their ultra-high-Q factors (Q>100 million).^{1-2,8-9} However, there are several notable differences between the two structures. Silica microspheres are free-standing, supported by a single optical fiber, whereas silica microtoroids can be fabricated on a silicon wafer in large arrays using a combination of lithography and etching steps. These differences influence which device is optimal for a given experiment.

Here, we present detailed fabrication protocols for both types of resonant cavities. While the fabrication of microsphere resonant cavities is fairly straightforward, the fabrication of microtoroid resonant cavities requires additional specialized equipment and facilities (cleanroom). Therefore, this additional requirement may also influence which device is selected for a given experiment.

Introduction

An optical resonator efficiently confines light at specific wavelengths, known as the resonant wavelengths of the device.¹⁻² The common figure of merit for these optical resonators is the quality factor or Q. This term describes the photon lifetime (τ_0) within the resonator, which is directly related to the resonator's optical losses. Therefore, an optical resonator with a high Q factor has low optical losses, long photon lifetimes, and very low photon decay rates ($1/\tau_0$). As a result of the long photon lifetimes, it is possible to build-up extremely large circulating optical field intensities in these devices. This very unique property has allowed these devices to be used as laser sources and integrated biosensors.¹⁰

A unique sub-class of resonators is the whispering gallery mode optical microcavity. In these devices, the light is confined in circular orbits at the periphery. Therefore, the field is not completely confined within the device, but evanesces into the environment. Whispering gallery mode optical cavities have demonstrated some of the highest quality factors of any optical resonant cavity to date.^{9,11} Therefore, these devices are used throughout science and engineering, including in fundamental physics studies and in telecommunications as well as in biodetection experiments.^{3-7,12}

Optical microcavities can be fabricated from a wide range of materials and in a wide variety of geometries. A few examples include silica and silicon microtoroids, silicon, silicon nitride, and silica microdisks, micropillars, and silica and polymer microrings.¹³⁻¹⁷ The range in quality factor (Q) varies as dramatically as the geometry. Although both geometry and high Q are important considerations in any field, in many applications, there is far greater leverage in boosting device performance through Q enhancement. Among the numerous options detailed previously, the silica microsphere and the silica microtoroid resonator have achieved some of the highest Q factors to date.^{1,9} Additionally, as a result of the extremely low optical loss of silica from the visible through the near-IR, both microspheres and microtoroids are able to maintain their Q factors over a wide range of testing wavelengths.¹⁸ Finally, because silica is inherently biocompatible, it is routinely used in biodetection experiments.

In addition to high material absorption, there are several other potential loss mechanisms, including surface roughness, radiation loss, and contamination loss.² Through an optimization of the device size, it is possible to eliminate radiation losses, which arise from poor optical field confinement within the device. Similarly, by storing a device in an appropriately clean environment, contamination of the surface can be minimized. Therefore, in addition to material loss, surface scattering is the primary loss mechanism of concern.^{2,8}

In silica devices, surface scattering is minimized by using a laser reflow technique, which melts the silica through surface tension induced reflow. While spherical optical resonators have been studied for many years, it is only with recent advances in fabrication technologies that researchers been able to fabricate high quality silica optical toroidal microresonators (Q>100 million) on a silicon substrate, thus paving the way for integration with microfluidics.¹

The present series of protocols details how to fabricate both silica microsphere and microtoroid resonant cavities. While silica microsphere resonant cavities are well-established, microtoroid resonant cavities were only recently invented.¹ As many of the fundamental methods used to fabricate the microsphere are also used in the more complex microtoroid fabrication procedure, by including both in a single protocol it will enable researchers to more easily trouble-shoot their experiments.

Video Link

The video component of this article can be found at <http://www.jove.com/video/4164/>

Protocol

1. Microsphere Fabrication

1. Select a small amount (approximately 5 inches) of optical fiber, strip ~1.5" cladding from one end and clean with either methanol or ethanol (**Figure 1a, b**).
2. If available, cleave the end with an optical fiber cleaver. If not available, cut with wire cutters or scissors such that ~0.5" is left. The advantage of using an optical fiber cleaver is that it produces a very smooth, uniform cut as in **Figure 1b**. Excessive roughness or defects from a cut may cause uneven reflow, lowering the quality factor of the resulting spheres.
3. Expose the cleaned fiber end to 3W of CO₂ laser power focused to a ~500 μ m diameter spot size for ~1 second (**Figure 1c, d, e**). This produces spheres ~200 μ m in diameter; however, the size can be tuned by increasing or decreasing the diameter of the optical fiber. Slightly adjusting the laser intensity may also be necessary to reflow larger or smaller spheres.

2. Microtoroid Fabrication

1. Design and make a photomask with dark, solid circles, in the spacing and diameter of your choice. It is important to note that the toroids produced will be 25-30% smaller than the circles on the mask. For example, a solid circle with a diameter of 100 microns will produce a toroid with a diameter of approximately 75 microns. Also, it is recommended to leave at least 1-2mm of space between each circle and at least 5mm of space between arrays of circles and around the edges of the mask. Since the sample wafers must be carefully handled with tweezers, it is important to leave space for the tweezers to grip without damaging the toroids. The extra space also provides room for a tapered optical fiber to couple light into the finished devices, and allows samples to be cut into smaller arrays more easily. For this procedure, we used a mask with rows of 160 μ m diameter circles ~1mm apart, with ~5mm of space between each row of circles. The finished toroids are approximately 110 μ m in diameter.
2. Begin with silicon wafers with a 2 μ m thick layer of thermally grown silica. Cleave the wafers to fit the desired microdisk pattern on the photolithography mask, leaving room for photoresist edge bead. Note that at the beginning of fabrication, it is usually most convenient to etch several arrays of circles on larger pieces of silicon wafers (~several cm x several cm). Larger wafers allow photolithography and BOE etching of more samples at a time, and are more easily handled with tweezers. Later, before the XeF₂ etching step, it is recommended to cleave the larger wafers into smaller arrays to allow faster, more uniform XeF₂ etching.
3. In a fumehood, thoroughly clean the wafers by rinsing with acetone, methanol, isopropanol, and deionized water. Blow the samples dry using a nitrogen or filtered compressed air gun, and place them on a hot plate set to 120°C for at least 2 minutes to dry.
4. After letting the wafers cool, place them in a flammable/solvent fumehood and expose to HMDS for 2 minutes using the vapor deposition method. A simple vapor deposition method: put a few drops of HMDS in a small 10ml beaker, and then cover the wafers and small beaker with a larger glass container to hold the vapor.
5. Place a sample on a spinner with an appropriately sized mount. Using a dropper bottle or syringe and filter, apply photoresist to the sample. Spin coat S1813 photoresist onto each sample for 5 seconds at 500rpm, followed by 45 seconds at 3000rpm. Edge bead removal is not needed if the wafer is sufficiently large so that the edge bead does not interfere with the patterning.
6. Soft bake the photoresist on a hot plate at 95°C for 2 minutes.
7. Using a UV mask aligner and the desired photomask, expose the photoresist-covered samples to a total of 80mJ/cm² of UV radiation.
8. Immerse the samples in MF-321 developer to remove the photoresist which was exposed to UV light. While developing, closely watch as the photoresist is removed from the wafer and dissolved. It is important to stir/swish the container constantly during this process to ensure the photoresist is removed uniformly. For the given parameters, the photoresist takes approximately 30 seconds to develop.
9. When most of the unwanted photoresist has dissolved in the developer, rinse the samples thoroughly under running water, gently blow dry the samples using a nitrogen or air gun, and inspect the samples with a microscope to ensure all undesired photoresist has been removed. If needed, the samples can be immersed again in developer; however, one should be careful not to overdevelop the samples as the desired photoresist patterns could also be damaged. (If the desired patterns are damaged or defective, the photoresist can be removed with acetone and steps 2.1-2.9 can be repeated again).
10. After developing, thoroughly rinse the samples in running water, gently blow dry the samples, and hard bake them on a hot plate at 110°C for 2 minutes. This step heats the photoresist above its glass transition temperature, reflowing the photoresist and partially repairing roughness which occurred during the developing process.
11. Using Teflon containers and the necessary protective equipment, immerse the samples in improved buffered oxide etchant (BOE). BOE contains HF, which etches the silica not covered by photoresist to form circular silica pads on the silicon wafer (**Figure 2a-c**). Improved buffered HF produces a smoother etch, minimizing roughness in the resulting silica circles. While it is possible to mix buffered HF starting with 49% HF, this can lead to highly variable results as typically only small quantities are made.
12. After approximately 15-20 minutes (depending on the patterns, sample sizes and number of samples), remove the samples from the BOE using Teflon tweezers. Carefully rinse the samples in running water. The silica has been removed when the samples become hydrophobic.
13. After etching, rinsing, and drying the samples, inspect them using an optical microscope. Check to make sure the desired patterns have been etched completely and all the unwanted silica has been removed. If needed, return the samples to the BOE for further etching. One should be careful not to overetch the samples, or the circular patterns underneath the photoresist may be damaged.

14. Once BOE etching is complete, thoroughly rinse the samples in deionized water and blow dry. If the samples are on large pieces of silicon wafer, it is also recommended to cut them (using a dicing saw or diamond scribe) into smaller pieces with individual rows of silica circles. Individual rows of circles are etched more quickly and uniformly in the XeF₂ etching step (2.16). Silicon dust produced by the cutting is removed during cleaning in the next step.
15. Remove the photoresist by rinsing with acetone, methanol, isopropanol, and deionized water, and dry the samples using a nitrogen gun and heating on a 120°C hot plate for at least 2 minutes.
16. Using a XeF₂ etcher, undercut the silicon beneath the circular silica pads to form silica microdisks (**Figure 2d-f**). The amount etched should be approximately 1/3 of the silica circle's size, so that the resulting microdisk's pillar is approximately 1/3-1/2 of the total disk diameter, as determined by inspection with an optical microscope. The number of XeF₂ pulses and the duration of each pulse depends on the amount of silicon in the chamber and the type of XeF₂ etcher used.
17. After XeF₂ etching, expose the samples to a focused CO₂ laser beam at approximately 12W intensity for ~3 seconds or until a smooth toroid is formed (**Figure 2g-i**). Depending on the exact size of the disk and the amount of XeF₂ undercut, a slightly higher or lower intensity and exposure time may be needed to form a microtoroid. It is important that the center of the laser beam and the center of the microdisk are aligned, so that the silica microdisk will form a smooth, circular microtoroid.

3. Representative Results

The microsphere and microtoroid devices can be imaged using both optical microscopy and scanning electron microscopy (**Figure 1d, e and Figure 2h, i**). In all images, the uniformity of the device surface is clearly evident.

To verify that the detailed approach creates ultra-high-Q devices, we also characterized the Q factor of several devices by performing a linewidth ($\Delta\lambda$) measurement and calculating the loaded Q from the simple expression: $Q = \lambda / \Delta\lambda = \omega\tau$, where λ =resonant wavelength, ω =frequency, and τ =photon lifetime. Representative spectra of each device fabricated using the previously detailed procedures^{1,9} and a comparison graph of several devices is shown in **Figure 3**. The quality factors of all devices are above 10 million, with the majority being above 100 million.

The spectrum of the microsphere was a single resonance, indicating that the light coupled into either the clockwise or counter-clockwise propagating optical mode. However, the spectrum of the toroid exhibited a split resonance, indicating that light coupled into both the clockwise and counter-clockwise modes simultaneously. This phenomenon occurs when there is a slight imperfection at the coupling site. By fitting the spectrum to a dual-Lorentzian, the Q factor of both modes can be determined. The split resonance phenomena can occur in both sphere and toroid resonators, but is more frequently observed in toroids as they are more susceptible to imperfections and have fewer optical modes compared to spheres.

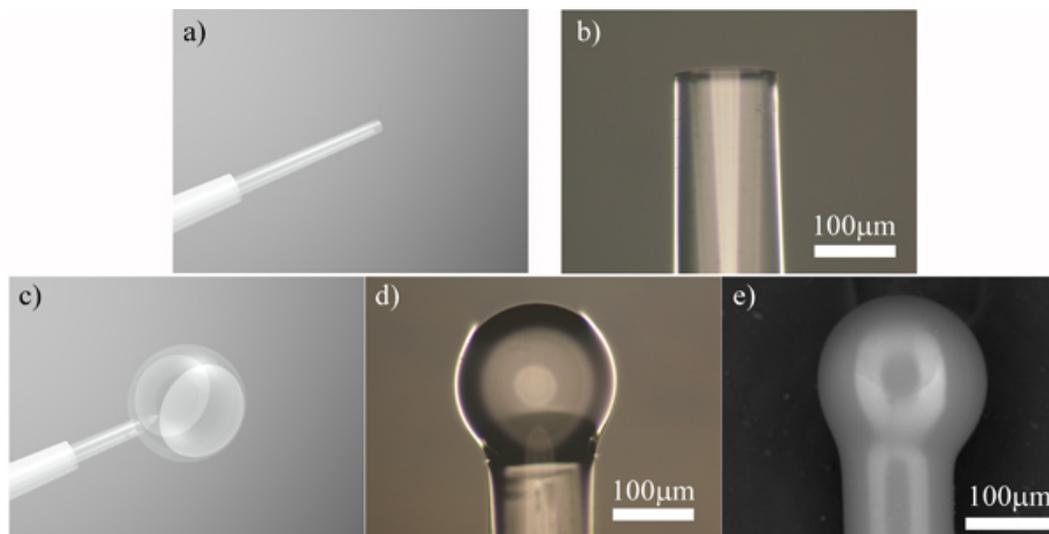


Figure 1. Flow chart of the microsphere cavity fabrication process. a) Rendering and b) optical micrograph of a cleaned and cleaved optical fiber. c) Rendering, d) optical micrograph and e) scanning electron micrograph of a microsphere resonator.

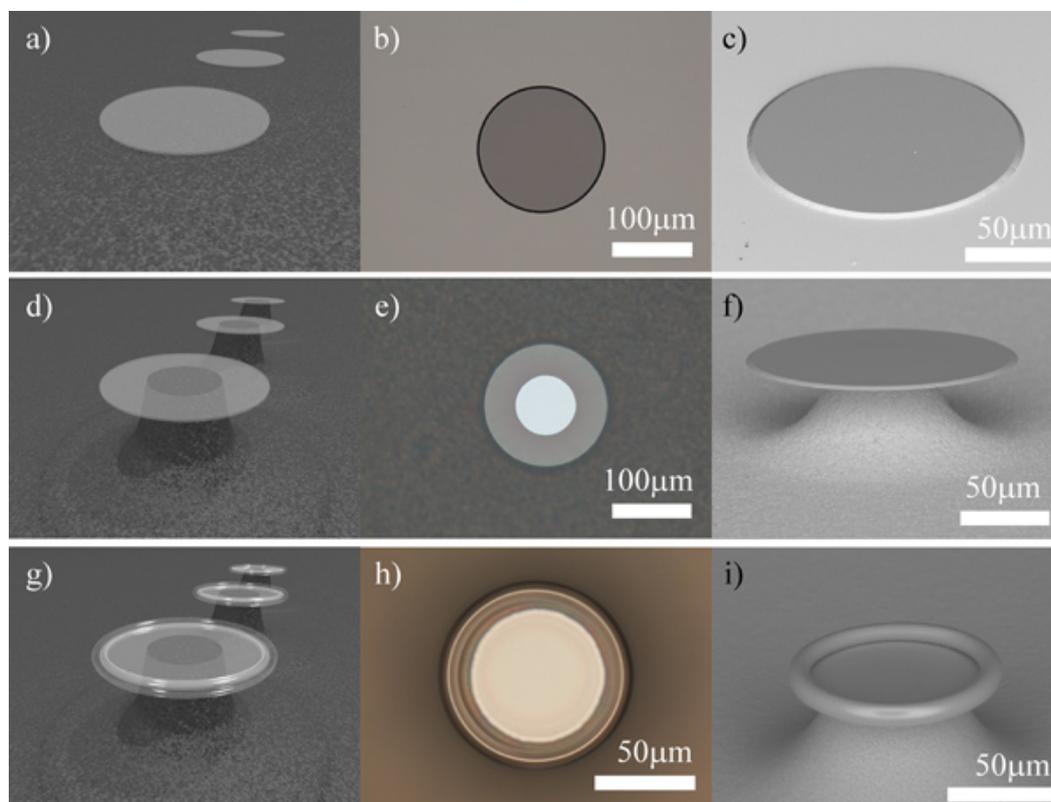


Figure 2. Flow chart of the microtoroid cavity fabrication process. a) Rendering, b) top-view optical micrograph and c) side-view scanning electron micrograph of the circular oxide pad, as defined by photolithography and BOE etching. Note the slight wedge-shape of the oxide that is formed by the BOE. d) Rendering, e) top-view optical micrograph and f) side-view scanning electron micrograph of the oxide pad after the XeF_2 etching step. Note that the oxide disk maintains the wedge-shaped periphery. g) Rendering, h) top-view optical micrograph and i) side-view scanning electron micrograph of the microtoroid cavity.

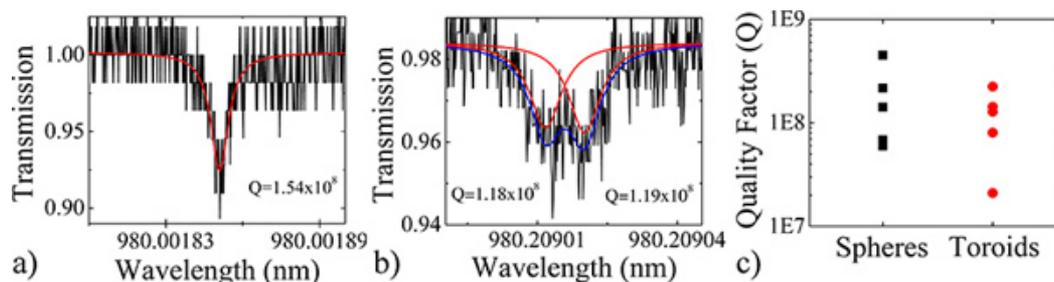


Figure 3. Representative quality factor spectra of the a) microsphere and b) microtoroid resonant cavities as determined using the linewidth measurement method. In very high Q devices, one may observe mode-splitting or a double peak, in which light reflects off a small defect and circulates in both clockwise and counterclockwise directions. c) Comparison graph showing the Q factors of several microsphere and microtoroid resonant cavities. [Click here for larger figure.](#)

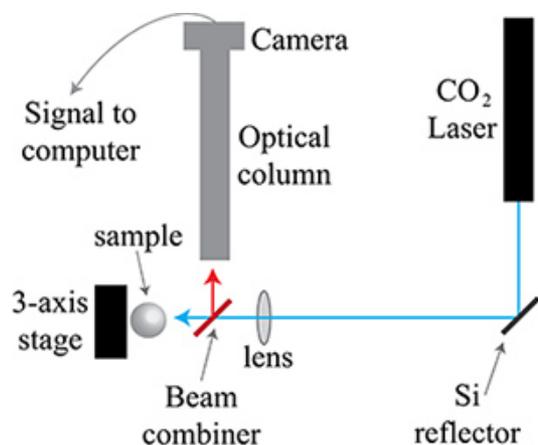


Figure 4. Schematic of the CO₂ laser reflow set-up. The CO₂ laser beam (solid blue line) is reflected and then focused on the sample. It passes through the 10.6 μm / 633 nm beam combiner, which transmits 10.6 μm and reflects 633 nm. The optical column images the reflection of the sample off of the beam combiner; therefore, the image is somewhat red. A list of the necessary parts for this setup is in **Table 4**.

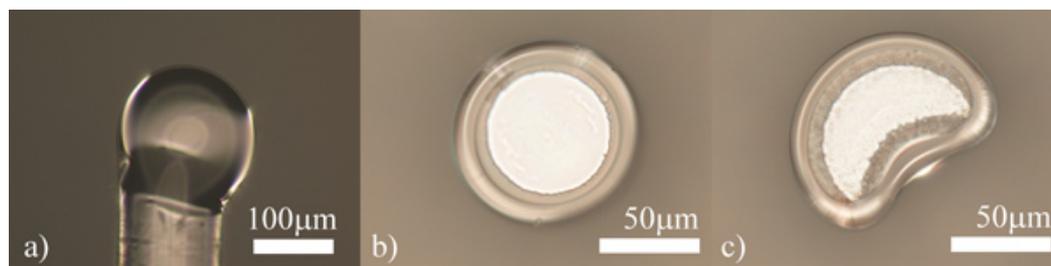


Figure 5. Incorrectly reflowed a) microsphere and b) microtoroid resonant cavities. Due to incorrect placement within the beam, the device is mal-formed. c) As a result of a poor photomask or poor lithography, the toroid is moon-shaped.

Discussion

As with any optical structure, maintaining cleanliness at every step of the fabrication process is of critical importance. As there are numerous textbooks written on the topic of lithography and fabrication, the suggestions below are not intended to be comprehensive, but highlight a few of the more common issues researchers have faced.¹⁹⁻²⁰

Because the uniformity of the microtoroid's periphery is determined by the uniformity of the initial disk, it is very important to pattern very circular disks. Common problems specific to the microtoroid are: 1) pixilation of photo-masks, 2) poor photolithography (under or over exposure, under or over developing, and rough or uneven etching), and 3) poor adhesion of the photoresist to the silica; here we address each issue individually.

It is very important to acquire high resolution photo-masks. While low resolution photomasks or ink-jet photomasks are readily available, these will result in "pixilated" or jagged circles which will not reflow correctly, resulting in non-circular toroids. The present protocols give UV exposure times for very specific photoresist film thicknesses at specific UV intensities. If different film thicknesses are used or if the photoresist is expired, then a different exposure time will be necessary. It is also advisable to calibrate one's photoaligner to ensure the correct UV exposure is given. Similarly, the time required in developer may vary as it is specific to the photoresist's film thickness and assumes that the photoresist is fully exposed. Finally, if the silica is not exposed to HMDS immediately before the photoresist is applied, the photoresist will not adhere well to the wafer. As a result, when the sample is etched using BOE, it will experience a severe and non-uniform undercut.

There is one other issue which also frequently arises with the toroid fabrication process and is related to the XeF₂ undercutting step. Because of the high degree of selectivity of XeF₂ for silicon over silica, the XeF₂ will not directly etch the native oxide which is inherently present on the silicon wafer. Therefore, it is important to make sure to minimize the potential growth of such an oxide and to further eliminate any further oxide growth by thoroughly purging the XeF₂ etch chamber with Nitrogen. If this is not done, the XeF₂ etch will be extremely rough or pocketed.

Additionally, in order to form a circular structure, it is very important to use an isotropic silicon etchant. While XeF₂ is the most commonly used etchant in the microtoroid fabrication process, there are others, such as HNA which is a mixture of hydrofluoric acid, nitric acid and acetic acid.²⁰ However, because it contains HF, it is not as selective for silicon as XeF₂ is, and the etching of the silica must be taken into account.

The CO₂ laser reflow process used must be done very precisely to successfully fabricate microspheres and microtoroids. One standard and simple reflow setup is shown in **Figure 4** with a list of parts in **Table 4**. There are many possible ways to build such a setup, and the layout and parts used can vary. However, the design must satisfy two important criteria. First, the distance between the sample and CO₂ laser's focusing lens must be equal to the lens's focal length, so that the sample is located in the focus of the laser beam. Second, the uniformity of the CO₂ laser across the spot and the placement of the device in the center of the spot are extremely important. This requires that all of the free space optics

are in alignment, and of course, free space optics can drift with temperature and humidity fluctuations. Example devices which were fabricated with incorrectly aligned optics are in **Figure 5**. To help avoid these alignment problems, cameras and stages can be used to allow easier, more accurate positioning of a sample under the beam. While using an optical table or vibration isolation is not required, having the reflow components integrated and secured on a breadboard can improve alignment.

If a CO₂ laser is not available, alternative reflow methods can be used. For the microsphere, a hydrogen torch could be used as an alternative method. If this approach is used, it is very important to follow all requisite safety protocols when building the reflow set-up, such as incorporating a flashback arrestor on the hydrogen tank and using a hydrogen torch, to eliminate the potential risk of an explosion. Typically, when this approach is used, a similar imaging system to that described for the CO₂ laser set-up is used for monitoring the reflow process. However, a hydrogen torch will not work for the microtoroid, as the melting temperature of silicon is less than that of silica. The CO₂ laser overcomes this problem, because silica strongly absorbs the laser light while silicon does not. Therefore, we have found that reflow with a properly aligned CO₂ laser beam allows us to obtain the most consistent reflow needed for high quality factor microsphere and microtoroid resonators.

The pair of methods presented here enable the fabrication of ultra-high-Q silica resonant cavities. As a result of their long photon lifetimes, these devices have numerous important applications, particularly within the biological sciences.

Disclosures

No conflicts of interest declared.

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